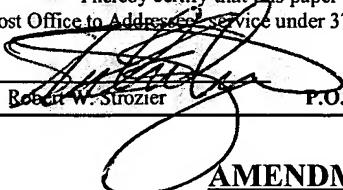




IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

APPLICANTS: **Wosik,Nesteruk and Xie** § ART UNIT NO.: **2831**  
SERIAL NO.: **10/532457 - PCT/US03/33933** § EXAMINER: **SHRIVASTAV, BB**  
FILED: **09/05/2006 - 10/24/2003** § DOCKET NO.: **96605/22US**  
  
FOR: **SUPERCONDUCTING ARRAY OF** §  
**SURFACE MRI PROBES** §

<b>EX 900187072 US</b> Express Mail Number	<b>CERTIFICATE OF MAIL BY EXPRESS MAIL</b>	<b>August 28, 2008</b> Date of Deposit
I hereby certify that this paper or fee is being deposited with the United States Postal Service "Express Mail" Post Office to Addressee service under 37 C.F.R. § 1.10 on the date indicated above and is addressed to the:		
 Robert W. Strozier		Commissioner of Patent
		<b>MS ISSUE FEE</b>
		P.O. Box 1450, Alexandria, VA 22313-1450
		<b>August 28, 2008</b> Date of Signature

AMENDMENTS AFTER ALLOWANCE

Applicants just discovered in preparing the formal drawing that the figure numbering in the Detailed Description of the Invention of the Specification is incorrect. Applicants' attorney uses a counter and incrementers to increment that Figure numbers so that Figures are not used twice. Applicants' attorney failed to reset the counter after the Brief Description of the Drawings. The last figure was 12 and the first figures in the Detailed Description of the Invention was 12 and should have been 1.

Applicants are submitting are herewith including amendments to the specification to correct these incorrect figure numberings.

Applicants are also attaching a substitute specification (with and without correction marking) for the convenience of the Office.

**AMENDEMENTS**  
**In the Specification**

[0056] Referring now to **Figures 121A&B**, the difference in an electric field distribution between the two-sided resonator designs of this invention, generally 1, and a single loop design, generally 150, are shown. When a pair of properly aligned loops or coils 102a and 102b having a dielectric substrate 104 interposed between them, then the resulting electric field 106 is confined within the dielectric substrate 104 and does not extend above or below resonator 100. Thus, such resonators 100 when used to image a body of an animal including a human, the generated electric field, being confined in the dielectric 104, does not penetrate the body. A similar design principle has been used for single superconducting coils. On the other hand, in the single loop design 150, the resulting electric field extends above and below the loop 150 and will penetrate into a body when used as an imaging resonator.

[0058] Referring now to **Figures 132A-C**, a preferred embodiment of a single resonator of this invention, generally 200, from which arrays can be constructed is shown to include a top coil 202 made of a conducting material, preferably a superconducting material and particularly an HTS material. The top coil 202 includes a discontinuity 204 and two outwardly extending protrusions or lands, tags or tabs 206 on opposite sides of the discontinuity 204. The resonator 200 also includes a bottom, opposing coil 208, also made of a conducting material, preferably a superconducting material and particularly an HTS material. The bottom coil 208 also includes a discontinuity 210 arranged to be maximally separated from the discontinuity 204 of the top coil 202, *i.e.*, the bottom or second coil 208 is rotated 180 degrees relative to the first or top coil 202, thus achieving maximal discontinuity separation. The resonator 200 also includes a dielectric substrate 212 interposed between the two coils 202 and 208 into which the generated electric field is confined. Unlike the top coil 202, the bottom coil 208 does not include tabs 206, but instead includes a pair of islands 214 of conductive material positioned in a capacitive relationship to the tabs 206, *i.e.*, the tabs 206 and the islands 214 with the dielectric 212 therebetween forming capacitors 215. The resonator 200 also includes a pair of contacts 216 with wires 218 bonded thereto so that the resonator 200 can be connected to a monitoring device such as an MRI imaging device or an NMR instrument. As shown in Figure 2A, the dielectric 212 extends into interior 220 of the resonator 200. Although this extension is not necessary as shown in **Figures 132D-F**, having the dielectric extend into the interior

regions 220 and out past the coils 202 and 208 is a manufacturing convenience and does not adversely affect resonator performance.

[0059] Referring now to Figures 132D-F, another preferred embodiment of a single resonator of this invention, generally 250, from which arrays can be constructed is shown to include a top coil 252 made of a conducting material, preferably a superconducting material and particularly an HTS material. The top coil 252 includes a discontinuity 254 and has a general horseshoe shape. The resonator 250 also includes a bottom, opposing coil 258, also made of a conducting material, preferably a superconducting material and particularly an HTS material. The bottom coil 258 also includes a discontinuity 260. Thus, in this preferred embodiment, the coils 252 and 258 are identical and are arranged so that the discontinuities 254 and 260 are maximally separated, *i.e.*, the bottom or second coil 258 is rotated 180 degrees relative to the first or top coil 252, thus achieving maximal discontinuity separation. The resonator 250 also includes a dielectric substrate 262 interposed between the two coils 252 and 258 into which the generated electric field is confined. Unlike the resonator design of Figures 132A-C, the resonator design of Figures 132D-F does not include capacitors formed from tabs 206 in the top coil 202 and islands 214 associated with the bottom coil 208. Instead, a pair of capacitors 264 are formed on the top coil 252 (or the bottom coil 258 not shown) at positions 266 on either side of the discontinuity 204 (210). Each capacitor 264 includes a dielectric layer 268 formed on a top surface 270 of the top coil 252 and a conductive layer 272 formed on top of the dielectric layer 268. The resonator 250 also includes a pair of contacts 274 formed on a top surface 276 of the conductive layer 272 having wires 278 bonded thereto so that the resonator 250 can be connected to a monitoring device such as an MRI imaging device or an NMR instrument. Unlike the resonator 200 of Figures 132A-C, the dielectric 262 of the resonator 250 does not extend into interior 280 of the resonator 250. Again, whether the dielectric 212 or 262 extends into the interior 220 or 280 is a matter of design and manufacturing convenience and has no adverse affect on resonator performance.

[0060] Referring now to Figure 132G, an expanded view of the capacitors 264 are shown, including a portion of the top coil 252, a portion of the bottom coil 258 and a portion of the dielectric 262. On the top surface 270 of the top coil 252 is formed the dielectric layer 268 and formed on top of the dielectric layer 268 is the conductive layer 272. Formed on the top surface 276 of the conductive layer 272 is the contact 274 with the wire 278 extending outward therefrom.

[0061] Referring now to **Figures 143A-D**, another preferred embodiment of a single resonator of this invention, generally 300, from which arrays can be constructed is shown to include a top coil 302 made of a conducting material, preferably a superconducting material and particularly an HTS material. The top coil 302 includes first and second discontinuities 304a&b and four protrusion or tabs 306 extending out from the discontinuities 304a&b. The resonator 300 also includes a bottom, opposing coil 308, also made of a conducting material, preferably a superconducting material and particularly an HTS material. The bottom coil 308 also includes two discontinuities 310a&b. In this design, the two coils are identical and the discontinuities of each coil are maximally separated. The two coils 302 and 308 are arranged so that all discontinuities 304a&b and 310a&b are maximally separated, *i.e.*, the bottom or second coil 308 is rotated 90 degrees relative to the first or top coil 302, thus achieving maximum discontinuity separation. The resonator 300 also includes a dielectric substrate 312 interposed between the two coils 302 and 308 into which the generated electric field is confined.

[0062] Like the resonator design of **Figures 2D-E**, the resonator design of **Figures 143A-D** includes a pair of capacitors 314 formed on the top coil 302 (or on the bottom coil 308 not shown) on the tabs 306. Each capacitor 314 includes a dielectric layer 316 formed on a top surface 318 of its tab 306 and a conductive layer 320 formed on top of the dielectric layer 318. The resonator 300 also includes a pair of contacts 322 formed on a top surface 324 of the conductive layer 320 having wires 326 bonded thereto so that the resonator 300 can be connected to a monitoring device such as an MRI imaging device or an NMR instrument.

[0063] As shown in **Figures 143A-D**, the dielectric 312 extends into interior 328 of the resonator 300. Although this extension is not necessary as shown in **Figures 2D-F**, having the dielectric 312 extend into the interior 328 and optionally out past the coils 302 and 308 is a matter of manufacturing convenience and does not adversely affect resonator performance.

[0064] Referring now to **Figures 154A-D**, another preferred embodiment of a single resonator of this invention, generally 400, having a substantially hexagonal shape from which arrays can be constructed is shown to include a top coil 402 made of a conducting material, preferably a superconducting material and particularly an HTS material. The top coil 402 includes three discontinuities 404a-c. The resonator 400 also includes a bottom, opposing coil 406, also made of a conducting material, preferably a superconducting material and particularly an HTS material. The

bottom coil 408 also includes three discontinuities 408a-c. In this design, the two coils are identical and the discontinuities of each coil are maximally separated, *i.e.*, each discontinuity is 120 degrees away from its nearest neighbor; provided, of course, that the current carrier distance between the discontinuities are substantially identical. The two coils 402 and 408 are arranged so that all discontinuities 404a-c and 410a-c are maximally separated, *i.e.*, the bottom or second coil 408 is rotated 60 degrees relative to the first or top coil 402, thus achieving maximum discontinuity separation. The resonator 400 also includes a dielectric substrate 410 interposed between the two coils 402 and 408 into which the generated electric field is confined. One advantage of the hexagonal resonators 400 arrays made from regular hexagons represent a maximum in resonator density for a given surface area.

[0065] Like the resonator designs of **Figures 2D-E** and **Figures 3A-D**, the resonator design of **Figures 154A-D** includes a pair of capacitors 412 formed on the top coil 402 (or on the bottom coil 408 not shown). Each capacitor 412 includes a dielectric layer 414 formed on a top surface 416 of its tab 406 and a conductive layer 418 formed on top of the dielectric layer 418. The resonator 400 also includes a pair of contacts 420 formed on a top surface 422 of the conductive layer 420 having wires 424 bonded thereto so that the resonator 400 can be connected to a monitoring device such as an MRI imaging device or an NMR instrument.

[0066] As shown in **Figures 154A-D**, the dielectric 412 extends into interior 426 of the resonator 400. Although this extension is not necessary as shown in **Figures 2D-F**, having the dielectric 412 extend into the interior 428 and optionally out past the coils 402 and 408 is a matter of manufacturing convenience and does not adversely affect resonator performance.

[0067] Referring now to **Figures 165A-B**, another preferred embodiment of a single resonator of this invention, generally 500, having a circular shape from which arrays can be constructed is shown to include a top coil 502 made of a conducting material, preferably a superconducting material and particularly an HTS material. The top coil 502 includes four discontinuities 504a-d and eight protrusion or tabs 506 extending out from the discontinuities 504a-d. The resonator 500 also includes a bottom, opposing coil 508, also made of a conducting material, preferably a superconducting material and particularly an HTS material. The bottom coil 508 also includes four discontinuities 510a-d. In this design, the two coils are identical and the discontinuities of each coil are maximally separated, *i.e.*, each discontinuity is 90 degrees away from its nearest neighbor. The

two coils 502 and 508 are arranged so that all discontinuities 504a-d and 510a-d are maximally separated, *i.e.*, the bottom or second coil 508 is rotated 45 degrees relative to the first or top coil 502, thus achieving maximum discontinuity separation. The resonator 500 also includes a dielectric substrate 512 interposed between the two coils 502 and 508 into which the generated electric field is confined.

[0068] Like the resonator designs of **Figures 2D-E**, **Figures 3A-D** and **Figures 4A-D**, the resonator design of **Figures 165A-D** includes a pair of capacitors 514 are formed on the top coil 502 (or on the bottom coil 508 not shown) on the tabs 506.

[0069] As shown in **Figures 165A-D**, the dielectric 512 extends into interior 516 of the resonator 500. Although this extension is not necessary as shown in **Figures 2D-F**, having the dielectric 512 extend into the interior 528 and optionally out past the coils 502 and 508 is a matter of manufacturing convenience and does not adversely affect resonator performance.

[0071] Referring now to **Figures 176A-C**, equivalent circuit diagrams for 1 discontinuity per coil resonator, for two 1 discontinuity per coil resonators and three 2 discontinuity per coil resonators. Looking at **Figure 6A**, a 1 discontinuity per coil resonator can be represented by an equivalent circuit, generally 600. The equivalent circuit 600 includes input outputs O/P1a&b, coupling capacitors CC with the coils represented by the inductor/capacitor loop **COIL**.

[0077] Referring now to **Figures 187A&B**, a preferred embodiment of a linear array comprising two resonators of this invention, generally 700, is shown to include a pair of resonators 702. Each resonator 702 includes a top coil 704 and an opposing bottom coil 706 with a dielectric substrate 708 extending out past the resonators 702. Each of the coils 704 and 706 has a single discontinuity 710 designed therein. The coils 704 and 706 are circular shaped and are arranged in a mirror imaged relationship. Each top coil 704 includes a pair of decoupling capacitors 712 formed thereon on each side of the discontinuities 710. The resonators 702 also include connecting capacitors (not shown). The array design 700 shows that the decoupling capacitors 712 can be formed on the same side of the resonator. Looking at **Figures 7C**, an alternative array 720 includes bottom coils 722, a dielectric 724, top coils 726, a second dielectric 728 and gold contacts 730. In this case, tabs 732 form the decoupling capacitors and wings 734 in combination with the gold contacts 730 from the connecting capacitors. Looking at **Figures 187D&E**, a preferred embodiment of a linear array comprising two resonators of this invention, generally 750, is shown to include a pair of resonators 752. Each

resonator 752 includes a top coil 754 and an opposing bottom coil 756 with a dielectric substrate 758 extending out past the resonators 752. Each of the coils 754 and 756 has a single discontinuity 760 designed therein. The coils 754 and 756 are square shaped. The resonators 753 are decoupled by a pair of decoupling capacitors 762 formed thereon on each side of the discontinuities 760 by tabs 764. The resonators 752 also include islands 766 which in conjunction with the tabs 764 can form sites for connecting capacitors (not shown).

[0078] Referring now to **Figures 198A&B**, a preferred embodiment of a linear array comprising three resonators of this invention, generally 800, is shown to include a pair of resonators 802. Each resonator 802 includes a top coil 804 and an opposing bottom coil 806 with a dielectric substrate 808 extending out past the resonators 802. Each of the coils 804 and 806 has a single discontinuity 810 designed therein. The coils 804 and 806 are square shaped and include tabs 812 and islands 814 forming decoupling capacitors 816 formed thereon on each side of the discontinuities 810. Each resonators 802 also include connecting capacitors with wires 818.

[0079] Referring now to **Figure 209**, another preferred embodiment of an MRI or NMR probe of this invention, generally 900, is shown to include a non-chained, planar or array 902 of a plurality of 2 discontinuity resonators 904 formed into a  $3 \times 3$  array. Each resonator 904 is made up of a  $3 \times 3$  array of top coils 911a-919a having tabs 923, 924, 926 and 927 and a  $3 \times 3$  array of bottom coils 911b-919b having tabs 933, 934, 936, 937 and a dielectric substrate 940 interposed therebetween. Overlapping portions of tabs 923, 924, 926, 927 933, 934, 936, and 937 form the decoupling capacitors as shown in Figure 7E. In the array 900, each nearest neighbor resonator may be oriented in a plane with a 90 degree offset orientation from its nearest neighbor resonators 904. Each resonator 904 also includes connecting capacitors 950 formed from dielectric layer 960 deposited on certain of the tabs 923, 924, 926 and 927 and conductive layer 953 and 954 deposited on the dielectric layer 960.

[0080] Referring now to **Figure 2110**, a preferred embodiment of an array, generally 1000, of hexagonal resonators 1002. Each resonator 1002 includes top and bottom coils 1004 and 1006 having tabs 1008 formed on a dielectric substrate 1010. Again, overlapping portions of the tabs 1008 on adjacent resonators 1002 form decoupling capacitors 1012. The resonators 1002 also include connective capacitors with contact 1014 formed on the top coils 1004. Again, the resonators are preferably made out of HTS and the arrays are preferably operated at or below their  $T_c$ . It should

be recognized that the array 1000 can also include other shaped resonators fill all portions of the rectangular surface or can be skewed so that the hexagonal packing is maximal.

[0081] Referring now to **Figure 2211**, a preferred embodiment of an MRI probe assembly of this invention, generally 1100, is shown to include a probe 1102 having a housing 1103, an array 1104 of resonators 1106 of this invention formed on a dielectric substrate 1108 along with pre-amplifiers 1110, one for each resonator 1106. The probe assembly 1100 also include a source for cooling 1112 in thermal contact 1114 with the probe 1102 to cool the array 1104 and pre-amplifiers 1110. The outputs of the pre-amplifiers 1110 are in electrical communication 1116 with an MRI scanner unit 1118. Preferably, the cooling source 1112 a cryogenic cooling device.

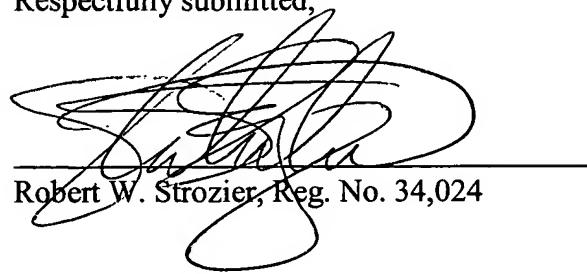
[0082] Referring now to **Figure 2312**, a preferred embodiment of an MRI apparatus of this invention, generally 1200, is shown to include a probe 1202 a housing 1203, having an array 1204 of resonators 1206 of this invention therein and positioned relative to a location 1208 on a human body 1210. Output signals from the resonators 1206 are transmitted along an output cable 1212 to an amplification unit 1214 including one amplifier for each resonator 1206. The outputs are then collected, processed and analyzed to produce an image on receiver device 1216. The probe 1202 is thermally connected via connection 1218 to a source of cooling 1220. The resonators 1206 receive NMR signals from sample body 1210 and transfer the signals to amplifier 1214. The signals may then be further communicated to external receiver 1206 where the data may be processed

[0022] The cryogenic housing 1203 may further comprise a heat conductive holder (not shown in the figures), which fixes the array 1204 in predetermined position in cryogenic housing 1203. The heat conductive holder is made out of heat conductive material, such as copper, sapphire, and the like. The source of cooling 1220 can be a cryogenic fluid circulation system where the connection 1218 is supply and return fluid line or a cold finger where the connection 1218 is simple thermal contact.

**The Commissioner is authorized to charge or credit Deposit Account 501518 for any additional fees or overpayments.**

Respectfully submitted,

Date: August 28, 2008

  
Robert W. Strozier, Reg. No. 34,024